Boundary element formulation of axisymmetric problems for an elastic halfspace

M.F.F. Oliveira^{a,n}, N.A. Dumont^b, A.P.S. Selvaduraf^c

^a Computer Graphics Technology Group, Department of Civil Engineering, Ponti"cal Catholic University of Rio de Janeiro, 22453 900 Rio de Janeiro, **Bita** ^b Department of Civil Engineering, Ponti"cal Catholic University of Rio de Janeiro, 22453 900 Rio de Janeiro, Brazil

elastic halfspace, given in terms of integrals of the Lipschitz...Hankel type, that satis"es in advance the

boundary condition of zero traction on the free surface and the decay of displacements in the far "eld.

Explicit equations for post-processing the results at internal points are provided, as well as adequate

numerical schemes to evaluate the boundary integrals arising in the method. This formulation can be easily

implemented in existing BE computational codes for axisymmetric fullspace problems, requiring only a few modi cations. Numerical results are provided to validate the proposed formulation.

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1. Introduction

The axisymmetric formulation in classical elasticity is useful for the analysis of problems in geomechanics [1,2], as well as contact problems for cylinders, spheres and circular plates [3..8]. Other applications involve the study of fracture mechanics phenomena and inclusions [5,9..11].

In particular, the BE method is advantageous for axisymmetric problems, since it reduces the analysis of the three-dimensional domain to a one-dimensional mesh discretization requiring only the evaluation of linear integrals. However, the fundamental solutions involved are more complex, requiring special considerations on their manipulation and integration to correctly evaluate the in"uence coef"cients arising in the boundary integral equations. Extensive surveys on the existing axisymmetric fundamental solutions are given by Wang and Liao [12,13], Wang et al. [14] and Wideberg and Benitez [15].

The BE method for axisymmetric elasticity was "rst formulated by Cruse et al. [16], using the fullspace fundamental solution derived by Kermanidis [17]. Several contributions to the formulation of the axisymmetric problem may be cited, such as the expansion of non-symmetric boundary conditions by Fourier series suggested by Mayr [18] and Rizzo and Shippy

[19,20

the number of unknown functions can be reduced from 12 to 6. These functions can be determined using (i) the compatibility conditions of displacements at the interface

u¦ðr

und ¼ _____

where G_E and \overline{G}_E are portions of the circumference of radius \quad E as depicted in Fig. 4.

za 0. On the other hand, for $z^{1/4}0$ the traction term t^{nd}_{ij} vanishes and only u^{nd}_{ij} presents singularity.

In this section, the integration cases identi"ed for G_{ia}^{t} and H_{ia}^{t} are grouped according to the position of P $\delta x, z^{0}$ -in relation to the part of the boundary along which the integration is carried out as well as to the axis of symmetry. The numerical schemes employed in this work to evaluate regular integrals, weakly singular integrals of logarithmic terms and the "nite part of singular integrals of order 1 =r are brie" presented in Appendix C.

4.1. Case 1:Pðx,z⁰l≩Gt

If the point P $\delta x, z^{0}$ does not belong to the portion of the boundary being integrated, as illustrated in Fig. 5, then r 4 0 and accordingly both G_{1a}^{t} and h_{ia}^{t} expressed in Eqs. (56) and (57) are regular and can be evaluated by the Gauss...Legendre quadrature rule [65]. For each portion of the boundary, these integrals can be rewritten in terms of the natural coordinate $ZA \frac{1}{2}1$; 1 as Z_{1}

where JoZÞ

Gauss...Legendre quadrature rule while the second integral has logarithmic singularity and should be evaluated by the weighted logarithmic Gauss quadrature rule [65]. Although the complete elliptic integral E(m) presents no singularity, its nonsingular approximation also includes logarithmic terms which are also isolated to enhance numerical convergence.

Owing to Eqs. (60)...(63), \dot{H}_{ia}^{t} as given by Eq. (57) also includes logarithmic terms in $t_{K_{ij}}^{nf} K dm Pand t_{E_{ij}}^{nf} E_{2} dm Pn \overline{m}$. Thus, their integration can be carried out by means of a regular integral and a weakly logarithmic singular integral, similar to the procedure proposed for G_{ia}^{t} . On the other hand, the integral of $t_{E_{ij}}^{nf} E_{1} dm Pexists$ only in terms of the "nite part, to be numerically evaluated by the scheme proposed by Dumont and Souza [67] for singular integrals in terms of order 1 =r over a curved boundary. This procedure employs the Gauss...Legendre quadrature and an additional correction term, as summarized in Appendix C. Hence, \dot{H}_{ia}^{t} can be given by

$$\begin{array}{l} {{{\bf{h}}_{ia}^{t}}^{t}}_{ia}^{t} & 2p \end{array}^{Z_{1}} \left(\begin{array}{c} {{}^{''}}\\ {}^{t} \\ {}^{t} \\$$

where Z^0 is the value of Z at the singularity point (which is either

1 or 1) and Z_m^g and w_m^g are the abscissae and weights of the Gauss...Legendre quadrature scheme for n_g points. In the above equation, the limit of $t_{E_i}^{nf} \Gamma N_a \delta Z_P \delta Z_P$ for Z- n^0 is dif"cult to obtain analytically and has been evaluated numerically by extrapolation. Alternatively, the elements of the matrix \hat{P}_{ia} that require the

Alternatively, the elements of the matrix \dot{R}_{ia} that require the evaluation of singular integrals can be obtained indirectly by r11(/0h)-4126

The complete elliptic integrals can be approximated as in Eqs. (62) and (63). Similar to the procedure presented for Case 2.1, one arrives at

Z₁ G^t_{1a} ¼ 2p u

$$\frac{2ck^{5}}{p\overline{k}^{4}A_{1}^{5}} = 6dk^{2} 2b \frac{c^{2}k^{2}}{A_{1}^{2}} \frac{8k^{4}}{\overline{k}^{2}} p \frac{1}{23} Edmb$$

$$A:11b$$

$$I_{113} \frac{4}{p\overline{k}^{2}A_{1}^{5}} = \frac{2ck^{3}}{3dk^{2}} 2bp\frac{2c^{2}k^{2}}{A_{1}^{2}} \frac{2k^{4}}{\overline{k}^{2}} p \frac{1}{3} Kdmb$$

$$\frac{2ck^{3}}{p\overline{k}^{4}A_{1}^{5}} 46dk^{4}p \overline{k}^{2}bp\frac{c^{2}k^{2}dk^{2}}{\overline{k}^{2}A_{1}^{2}} \frac{2bd\overline{k}^{2}p 8k^{4}}{\overline{k}^{2}} Edmb$$

$$A:12b$$

 $S_{rrrz}^{nd} \frac{m}{4p \delta 1} \frac{1}{n^{b}} \frac{1}{x} sign \delta P_{p} (1_{111} p \delta P_{5} z p z^{0} P_{112})$ sign $\delta P_{2} z z^{0} (1_{113} p sign \delta P_{2} P_{012} \delta 3 z p z^{0} P_{013})$ sign $\delta P_{2} z z^{0} (1_{014} \delta P_{112} \delta P_{112} \delta P_{112} \delta P_{112})$ where

S			
JöZ⊳¼	$\frac{dr}{dZ}^{2}$ b	$\frac{dz}{dZ}^{2}$	ðC:2Þ

is the Jacobian transformation between the global and natural coordinate systems. The coef"cients Z_m^g and w_m^g are the abscissas and weights of the Gauss...Legendre quadrature rule for n_g points within the interval δ 1;1P, which suf"ce to exactly evaluate the integral of a polynomial of order 2 n_g 1.

C.2. Weakly singular integral of logarithmic terms

Let fð,zÞbe a regular function and

where \overline{m} is given by Eq. (C.8) and

 $E_1 \overline{m} \triangleright \frac{1}{4} 1 \flat a_1 \overline{m} \flat b a_4 \overline{m}^4$

 $E_2 \overline{dm} P \frac{1}{b_1} \overline{m} p \quad p \quad b_4 \overline{m}^4$

are the polynomials whose coef"cients are given by

a₄ ¼ 0:01736506451, b₄ ¼ 0:00526449639

ðC:20Þ

ðC:19Þ

The polynomial approximation of E(m) presents no singularity, since $E_2 \overline{\sigma}\overline{m}$ b has no free coef"cients, according to Eq. (C.18). However, the presence of ln \overline{m} causes the integrand of Eq. (C.17) to be non-analytical, which requires a special numerical treatment.

In a manner similar to that used in the previous section, the following expression can be obtained for the numerical evaluation of the weakly singular integral given by Eq. (C.17) $_7$

$$f \tilde{\sigma}_{z} z E \delta m P dG$$

$$G$$

$$\chi_{9}$$

$$f \delta Z P E_{1} \delta m P p 2 E_{2} \delta m P ln \frac{1}{2^{p}} \frac{Z'Z}{m} J \delta Z P$$

$$Z'_{2} Z_{m}^{w} W_{m}^{g} \delta C: 21 P$$

$$4 \frac{\chi_{1}}{m \chi_{1}} f \delta Z E_{2} \delta m P h Z \delta Z P_{Z'_{2} Z_{m}} W_{m}^{l} \delta C: 22 P$$

for Z given by Eq. (C.6).

C.3. Cauchy principal value of the singular integral of order 1=r

Let f $\mathring{\sigma}$,z $\stackrel{\text{bbe}}{=}$ a regular function and r $\mathring{\sigma}$,z $\stackrel{\text{bt}}{=}$ the distance between the points P $\mathring{\sigma}$,z $\stackrel{\text{be}}{=}$ and Q $\mathring{\sigma}$,z $\stackrel{\text{boundary}}{=}$ G $\mathring{\sigma}$,z $\stackrel{\text{be}}{=}$ The strongly singular integral

has to be evaluated for the case $r \circ 1 \vdash \frac{1}{20}$ or $r \circ l \vdash \frac{1}{20}$. This integral may be obtained as a sum of a Cauchy principal value and a discontinuous term as

The evaluation of the discontinuous term c of the strongly singular integrals appearing in the boundary element formulations is addressed in Section 3.2.

The Cauchy principal value is best evaluated in terms of two "nite-part integrals, denoted by adjacent to the singularity point $r \check{\sigma}$, zP 1⁄20.

In what follows, the integration scheme proposed by Dumont and Souza [67] is used. Using the notation of Eq. (C.6), the regular function can be expanded as a Taylor series to obtain the following normalized integral of Eq. (C.23) over the curved boundary G

$$\frac{Z}{G}\frac{f\tilde{\sigma},zP}{r\tilde{\sigma},zP}dG^{1/2} = \frac{Z}{2^{1/2}}\frac{1}{r\tilde{\sigma}}\frac{f\tilde{\sigma}ZP}{T}dG^{1/2} = \frac{Z}{2^{1/2}}\frac{1}{r\tilde{\sigma}}\frac{f\tilde{\sigma}ZP}{T}dG^{1/2} = \frac{1}{r\tilde{\sigma}}\frac{f\tilde{\sigma}ZP}{T}dG^{1/2} = \frac{1}{r\tilde{\sigma}}\frac{f\tilde{\sigma}Z$$

The resulting quadrature rule for evaluating Cauchy•s principal value of the strongly singular integral of (C.23) is given by

$$\frac{Z}{_{G}}\frac{f\tilde{\sigma},z^{\mathbf{b}}}{r\tilde{\sigma},z^{\mathbf{b}}}dG = \frac{X_{9}}{_{m \ 124}} \frac{f\tilde{\Delta}^{\mathbf{b}}}{r\tilde{\Delta}^{\mathbf{b}}} \frac{dZ^{\mathbf{b}}}{Z_{24}Z_{m}^{\mathbf{a}}} w_{m}^{\mathbf{g}}$$

where

The above scheme, that employs the Gauss...Legendre quadrature rule and an additional correction term, evaluates exactly this integral for a polynomial function of order 2 n_g . Other numerical integration schemes for the strongly singular integral can be used [72,73].

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